This part should only be installed by personnel who have the necessary skill, training and tools to do the job correctly and safely. Incorrect installation can result in personal injury, vehicle damage and / or loss of vehicle control.

PART NO. 75210

Instruction sheet **REAR SHIM & BOLT KIT**

Plan Ahead - Read All Instructions <u>BEFORE</u> installing part.

Check for loose or worn parts, proper tire pressure, and odd tire wear patterns before beginning alignment.

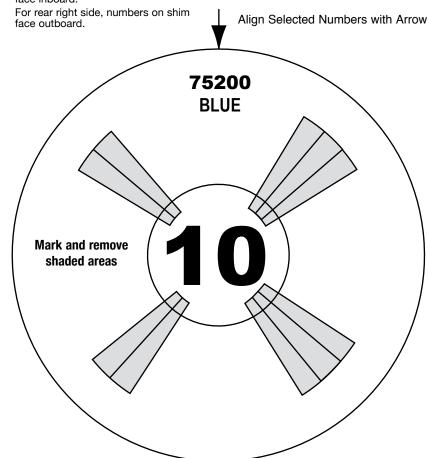
- 1. Prior to taking an alignment reading, inspect rear hub mounting area. Remove any existing alignment shims.
- Record initial alignment readings and 2. determine amount of camber and toe change required.
- Raise rear of vehicle and securely support. З.
- Remove rear tire and wheel assembly. 4
- Remove brake pipe retainer clip. 5.
- Remove 4 hub mounting bolts and pull 6. backing plate and drum assembly from axle beam. Support drum assembly to avoid stress on brake pipe and wiring. NOTE: Disassembly of drum brakes is typically not required.
- 7. Clean all contact surfaces.
- 8. Determine EZ-Shim[™] settings using included chart.
 - Choose desired toe change from left Α. side of chart and desired camber change from top of chart.
 - В. Locate box at intersection of desired settings. Numbers listed in box correspond to upper and lower shim disc positions (either number can be on upper or lower part of shim). If ideal box is empty, select a nearby box that offers best possible adjustment.

NOTE: Toe is always more critical than camber.

- 9. Mark areas of shim to be removed. Spin shim discs to align numbers Α.
 - designated from chart and mark these numbers' position using a marker.
 - B. Place shim on template with numbers facing up. Align ink mark on shim with top arrow on template.
 - C. Mark areas to be removed as indicated on template.
- 10. Using SPC# 75915 or equivalent cutter. and coming from inside of shim, snip both sides of marked areas just enough to break connection.
- NOTE: Wear safety glasses when cutting and removing marked areas.
- 11. Remove marked areas while firmly supporting shim adjacent to cut region.
- 12. Install shim in proper orientation.
 - For rear left side, numbers on shim A. face inboard.
 - B. face outboard.

- 13. Reassembly backing plate and drum assembly using supplied extended hub bolts. Each bolt should be torqued to manufacturer's specification plus 15%. Begin at thinnest part of shim and proceed in a cross pattern. Torque all bolts to 1/3 of torque value, then all bolts to 2/3 of torque value, then all bolts to full value.
- 14. Reinstall tire and wheel assembly and lower vehicle.
- 15. Complete alignment and road test vehicle. NOTE: Re-check bolt torque every 28,000 miles (50,000 kms).

Always check for proper clearance between suspension components and other components of vehicle.



Alignment Settings Chart on Back





4045 Specialty Place • Longmont, CO 80504 • (303) 772-2103 • Fax: (303) 772-1918 www.specprod.com • Email: info@specprod.com · Toll Free Technical Hot Line: 1-800-525-6505

©2023 Niwot Corp. dba Specialty Products Co® • Printed in U.S.A. • Form No. 75210INS • Rev. A ECN#3140

		DECIMAL INCHES	FRACTIONAL INCHES	DECIMAL DEGREES	DEGREES/MINUTES Grados/Minutos Grad/Min•degres/Min	5	STL	JRZ	ZÄI										ria Dn								ROS	6S/	٩GI	<u>E</u>
				DECI	GRAI	$1\frac{1}{2}$	PO9	SITIV 1 ¹ / ₄	'E・F 1	POSI	TIVC	$\mathbf{D} \cdot \mathbf{P}$	0SIT	۱V •	POS		1 8	0	1 8	1EG/	ATIV 3 8	E • N	EGA	TIV	O・N ⁷ / ₈	EGA	רוע - 11	$1\frac{1}{4}$	GATI 1 ³ / ₈	V 1 <u>1</u> 2
		FR/		DNAL DE		1.50°		4 1.25°	1.12°	1.0°	8 .88°.	4 .75°	8 .62°	2 .50°	8 .38°	4 .25°	8 .12º	0	8 .12°	4 .25°	8 .38°	2 .50°	8 .62°	4 .75°	8 .88°	1.0°	1.12°	4 1.25°		1.50°
		GRAD	DEG •DEG	REES•G RES/M	RADOS NUTES	1°30'	1º22'	1º15'	1º7'	1º6'	52'	45'	37'	30'	22'	15'	7'	0	7'	15	22'	30'	37'	45'	52'	1º6'	1º7'	1°15'	1º22'	1°30'
		.75	<u>3</u> 4	1.50°	1°30'											31 31	31 30	30 30	30 29	29 29										
		.72	23 32	1.44°	1º26'	_							00	32 32	32 31	32 30	32 29	32 28	31 28	30 28	29 28	28 28 29	07							
	٨	-68	1 <u>1</u> 16	1.36°	1º22'							34	33 33 34	34 31 35	34 30	34 29 34	33 28	33 27	32 27	31 26 32	30 26	29 26 30	27 27 28	27						_
	ΤI	.65	21 32	1.30°	1º18							33 35	32 35	30	35	28 35	34		33	26 32	31	25	26 26 29	26 28						_
	o s	.62 .59	5 8 19	1.25° 1.19°	1º15' 1º11'						35	32 36	31 36	36	29	28	27 35	34	26 33	25	25	31	25 30	25 29	27					_
	٩	.55	19 32 9 6	1.13	1º7'	-				35	33 36	31	30 37	29	36	36	27 35	26	25 34	33	32	24	24 30	24	25 28	26				_
	>	.53	16 17 32	1.06°	1º4'					34 35	32 37	37	30	37	28 37	27	26 36	35	25 34	24	24 32	31	23	29	24 28	25 25				-
	Т	.50	32 1 2	_99°	59 '				36 35	35 37 33	32	31 38 30	38 29	29	28	37 27	26 36 25	25	24 35 24	33 23	23	23	31 22	23 30 22	23	25 27 23	25 24			
	0 S I	.47	2 15 32	.94º	56'				37 34	00	38 32	38 31	23	38 28		37 26	25		24	34 23		32 22	~~~	29 22	28 22	20	23 26			
	Р	.44	<u>7</u> 16	-88°	52"			36 36	-	38 33	-	39 30	39 29		38 27		37 25	36 24	35 23		33 22		31 21	30 21		27 22		24 24		
		.41	1 <u>3</u> 32	.82°	49 '				38 34	39 32	39 31			39 28	39 27	38 26				34 22	33 21	32 21			29 21	28 21	26 22			
RIACION DE LA CONVERGENCIA FICATION D'ANGLE DE PARALLÉLISME	νo	.38	3 8	.75°	45			38 35	39 34		31 0	30 0	29 0			39 26	38 25	37 24	35 22	34 21			31 20	30 20	29 20		26 21	25 22		
	ΤI	.35	11 32	.69°	41'		37 37	38 36	33 0	32 0				28 0	27 0		38 24	37 23	36 22		33 20	32 20				28 20	27 20	22 24	23 23	
	s	.31	<u>5</u> 16	.62°	37		39	39 35 35	34 0	32 1 33	31 1	30 1 30	29 1	28 1	27	26 0 25	39 25 39	38	35 21 36	34 20 35	33	32 19	31 19	30 19 30	29 19	28 19 27	26 20	25 21 25	24	_
	Ρ0	.28	9 32	.55°	33		36 38	0	34	1	32	2	29	28	1	0 26	24	23	21	20 34	19	32	31	18 29	28	19	26	20	21 22	_
		.25	1 4 7	.49°	29		38 36	35	1	33	2	2	2 30	2	27	1 25	24	38	36	19 35	33	18	18 30	18	18	27	19	25	22 21	_
	νE	.22 .19	7 32 3	_43° _38°	26' 22'		0 39	1	34	2	32	31	3	29	2 28	1 26 2	0	22	20	19 34	18 32	31 17	17	29	28	18	26	19	20 21	_
	Т	.16	3 16 5 32	.32°	19'		38 37	35	2	33 3	3	3 31	30	3 29	3	27	24	39	36	18 33	17	31	30	17 29	17	27	18	25	22 23	_
	s o	.12	32 <u>1</u> 8	.25°	15'	39 39	0 38	2	34 3	3	33 4	4 32	4	4	28 4	3 26 3	1	22 39 21	19	17 34 17	32	16	16	16 28	27 16	17	26 17	18	20 22 20	21 21
	Р	.09	8 3 32	.19º	11'	39	0 37 1	36 2	35 3	34 4	4	4 32 5	31 5	30 5	29 5	3 28 5	25 3	21	35 17	32 15	16 31 15	30 15	29 15	16 28 15	10	26 16	25 17	24 18	20 23 19	21
		.06	<u>1</u> 16	.12º	7'	39 0	37 2	36 3			33 5		32 6	31 6	30 6	29 6	27 5	21 0	33 15	31 14	30 14	29 14	28 14		27 15			24 17	23 18	21 20
		.03	<u>1</u> 32	.06°	4'				35 4	34 5		33 6		32 7	31 7	30 7	28 7		32 13	30 13	29 13	28 13		27 14		26 15	25 16			
		0	0	0	0	0 0	38 2	37 3	36 4	35 5	34 6		33 7	32 8		31 9	30 9		30 11	29 11		28 12	27 13		26 14	25 15	24 16	23 17	22 18	20 20
		.03	<u>1</u> 32	.06°	4				36 5	35 6		34 7		33 8	33 9	33 10	33 12	10	27 8	27 10	27 11	27 12		26 13		25 14	24 15			
	٨	-06	<u>1</u> 16	.12º	7'	1 0	38 3 39	37 4 38	37	36	35 7	35	34 8 35	34 9 35	34 10 35	34 11 35	35 13 37	19 0	25 7 23	26 9 25	26 10 25	26 11 25	26 12 25	25	25 13	24	23	23 16 22	22 17 21	20 19
₹₫	ΤÌ	.09	3 32	.19°	11'	1	3	4	5 37	6	36	8 36	9	10	11	12 37	15	19	5	8	9	10	11	12	24	14	15	16	17 20	19
Ľ₹	GА	.12	1 8 5	.25°	15	1	2 0 3	38	6	37 7	36 7	8 36	36	36	36 12	14 37	39	1 18	21	23 6 23 7	24 8	24	24	24 12 24	24 13	23 13	23 14	22	18 20	19
д. Д	NEG	.16 .19	5 32 3 16	.32° .38°	19' 22'		0 2 1	5	38	7	37	9 37 9	10	11 37	37	13 38	16	1	4	7 22 6	23	9 23	10	11 23	23 12	13	22 14	15	17 19	-
ΑN		.22	16 7 32	.43°	26'		1 4 0	39 5	6	38 7	8	9	37 10	11	12 38 13	14 39 15	16 0	18 2	20 4	6 21 5	8 22 7	9	23 10	11	12	22 13	14	21 15	18 20 16	
TOE CHANGE • VARIACION DE LA CON SPURÀNDERUNG • MODIFICATION D'ANGLE	>	.25	32 1 4	_49°	29'		2 2	5	39 6	,	38 8	38 9	38 11	38 12	-10	39 14		-	Ļ	21 6	,	22 8	22 9	22 11	22 12	10	21 14	.5	18 18 18	\neg
	ATIV	.28	4 9 32	.55°	33'		4	5 0		39 7		38 10			39 13	15 0	16 1	17 2	19 4	20 5	21 7			22 10		21 13		20 15	19 16	
	ЕG	.31	<u>5</u> 16	.62°	37			5 1	6 0	39 8	39 9	39 10	39 11	39 12		14 0	15 1		19 5	20 6		21 8	21 9	21 10	21 11	21 12	20 14	19 15		
	z	.35	11 32	-69°	41'		3 3	4 2	7 0	8 0				12 0	13 0		16 2	17 3	18 4		20 7	20 8				20 12	20 13	18 16	17 17	
	•	_38	3 8	_75°	45			5 2	6 1	0	9 0	10 0	11 0	10	10	14 1	15 2	16 3	18 5	19 6	10	10	20 9	20 10	20 11	10	19 14	18 15		
	νo	.41	13 32	_82°	49			4	6 2	8 1 7	9 1	10	11	12 1	13 1 13	14 2	15	16	17	18 6	19 7 18	19 8	19	19	19 11	19 12 18	18 14	16		_
	ATIV	.44	<u>7</u> 16	-88°	52			4	6	2	8	1	1	12	2	14	3	4	5	17	7	18	9	10 18	18	13	17	16		_
	5	.47 .50	15 32 1	.94° .99°	56' 59'	_			3 5	7 3	8 2	9 2 10	11	12 2		3 13	15		16	6 17		18 8	18	11 18	18 12	17	14 16			_
	Ш Z	.50	1 2 17 32	1.06°	1º4'	-			4	3 5 5	8	2 9 3	2	11 3	12 3	3	4	15 5	5 16	7	17 8	17 9	9	10 17	17 12	13 15 15	15			_
		.56	32 9 16	1.13°	1º7					5 6 5	3	3	10	3	12	13	4 14 5	5	6 15 6	16 7	16	9	17	11	16	15				-
	νE	.59	16 19 32	1.19°	1º11					Э	4 7 5	9 4	3 10 4	11 4	4	4	5 13 5	14 6	6 15 7	/	8	16 9	10 16 10	16 11	12 15 13	14				\neg
	ATI	.62	32 5 8	1.25°	1º15'							8 5	9 5	-	11 5	12 5	13 6	5	7 14 7	15 8	15 9		15 11	15 12						\neg
	G	.65	8 21 32	1.30°	1º18'							7 6	8 6	10 5	-	12 6				14 8	-	15 10	14 12	14 13						
	ΝE	.68	11 16	1.36°	1°22'								7 7	9 6	10 6	11 6	12 7	13 7	13 8	14 9	14 10	14 11	13 13							
		.72	23 32	1.44°	1º26'									8 8	9 8	10 8	11 8	12 8	12 9	12 10	12 11	12 12								
		.75	<u>3</u> 4	1.50°	1°30'											9 9	10 9	10 10	11 10	11 11										

TOE CHANGE · VARIACION DE LA CONVERGENCIA